

PROTECTING BESSs WITH COMPREHENSIVE STRATEGY

Battery Energy Storage Systems (BESSs) demand a comprehensive circuit protection strategy

INTRODUCTION

Recent growth in renewable energy generation has triggered a corresponding demand for battery energy storage systems (BESSs). The energy storage industry is poised to expand dramatically, with some forecasts predicting that the global energy storage market will exceed 300 gigawatt-hours and 125 gigawatts of capacity by 2030. Those same forecasts estimate that investments in energy storage will grow to \$103 billion over that period. At the same time, the cost per kilowatt-hour of utility-scale battery systems is likely to drop to less than half of today's cost, making controlling system costs critical.

Today's battery systems aren't just designed to serve as local power backups, such as the systems used to power critical facilities including hospitals, data centers when the normal power source fails. BESSs also offer other benefits and ancillary services, including load-leveling, spinning and regulation reserves, T&D deferral, and frequency regulation, which when captured as a value stack maximizes this as a valued asset to utilities. Today's BESSs are increasingly designed to feed local micro-grids to supply power to the local area when the demand rises. They store electrical energy produced by solar or wind power generators, then inject that energy back into the grid when needed.

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BESS CIRCUIT PROTECTION

As the power density of modern lithium-ion batteries grows, BESS integrators are striving to offer their customers more power in a smaller footprint. However, with higher power levels, circuit protection becomes increasingly important.

Renewable energy providers are incorporating new generations of high-efficiency power semiconductor devices into their systems to control power in inverters and converters. Because these are sensitive electronic devices, they require robust protection against energy surges. The design of BESSs can still be considered to be in its infancy, given that the technologies that go into them are evolving rapidly. As a result, many of the electrical engineers integrating those solutions are seeking guidance in selecting and implementing appropriate circuit protection strategies.

A comprehensive circuit protection strategy is crucial to meeting BESS integrators' most critical objectives:

- > To prevent costly service interruptions to end-users with critical uptime requirements, such as hospitals, industrial processing plants and data centers. For example, the cost of data center downtime is in the range of \$8000 per minute.
- > To prevent revenue losses for renewable energy suppliers.
- > To prevent power disruptions to the local area.
- > To protect the workers who will install and maintain the BESSs that the integrators will design.
- > To prevent damage to the BESS equipment itself, which would jeopardize the sizable investment that the end-users or renewable energy suppliers have made.
- > To provide grid stability as generation is additionally from renewable sources.

Electrical faults within a BESS can pose significant hazards to workers, including the risk of electric shocks, chemical/ electrolyte burns from the batteries, and the release of toxic or explosive gas. The three main areas of concern are protection against electrical overcurrents, ground faults and arc-flash hazards.



OVERCURRENT PROTECTION

Inverter protection is one of the most important facets of BESS circuit protection. Inverters are typically-although not alwayslocated outside of the trailer or other enclosure in which the banks of batteries are housed. A DC/AC inverter converts DC output from batteries into a utility frequency alternating current (AC) that can be fed into a commercial electrical grid. However, a BESS also allows storing the DC current generated by renewable energy sources to a bank of batteries. Later, when there's a demand for that stored power, a DC/AC inverter converts the DC battery power into AC power that can be exported to the grid.

In order to provide the longest possible battery discharge times, BESS designers are building in larger and larger battery banks. Each of those batteries represents an energy source. Any fault in the system can lead to dumping a massive amount of energy all at once, and all the dangers to people and equipment that could pose.

A wide range of fuses are available to handle a variety of current overload applications. High-speed fuses are the usual choice **Figure 1.** Littelfuse PSR Series High-Speed Square-Body Fuses for these DC ESS applications because they are much smaller, are frequently used for overcurrent protection of inverters faster and less expensive than DC circuit breakers. The maximum because of their compact design, fast response to short circuit interrupting rating for circuit breakers tops out at about 25,000 to 30,000 amps. In contrast, the latest generation of high-speed fault currents, and high interrupting ratings. fuses (such as Littelfuse PSR Series High-Speed Square-Body Fuses) (Figure 1) can interrupt up to 150 kA of DC current (or 200 These fuses are also invaluable for protecting a BESS's DC kA AC) in a much smaller footprint than a DC circuit breaker.

High-speed fuses are designed to operate about 24 times faster than conventional fuses in order to protect sensitive power semiconductor devices (such as diodes, triacs, IGBTs, SCRs, MOSFETs and other solid-state devices) that are built into inverters, UPSs, battery management devices, and other systems by reducing peak let-through current and let-through energy (I2t).

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batteries. Each battery is protected by DC fuses at the positive and negative terminals to isolate the battery during any internal short-circuit condition. DC combiners, where the outputs from multiple battery racks are combined to feed the inverter, are critical locations that are susceptible to high DC overcurrent faults. Typically at this location, output strings from batteries are protected by DC fuses with the highest possible DC



GROUND FAULTS

A variety of factors can contribute to the development of ground faults. These factors include insulation or component degradation over time (often as a result of overvoltage or overtemperature), humidity/ moisture, rodents, dust accumulation between live parts of the system, and human error. Unless an appropriate ground-fault device is used, low-current ground faults can often go unrecognized.

BESSs are typically ungrounded systems. The system may remain in operation after the first ground fault, resulting in higher voltage on the unfaulted bus with reference to ground but with no current flow. However, subsequent ground fault on the opposite bus can have catastrophic consequences from both an equipment-protection and worker-safety perspective. A second ground fault on an ungrounded system may constitute a phase-to-phase fault that can result in arcing, fires and severe damage or injuries. Most electrical faults, including arc flashes, begin as ground faults and so detecting these faults early is essential so they can be addressed before serious damage or injury occurs.

For ungrounded BESS systems, designers can choose from three options for ground-fault detection for the DC side:

- 1. Active insulation monitoring. This approach involves injecting a low-level signal that seeks the lowest-resistance path back to the relay through ground. The leakage current returning to the relay is directly proportional to the insulation of the system to ground. This method is attractive, but has some significant challenges, including difficulty in locating the exact fault location, susceptibility to system capacitance and interference of the active signal with other components of the electrical system.
- 2. Passive voltage monitoring with respect to ground. This method does not inject an active signal; instead, it monitors the voltage of each side of the DC bus (or each phase of the AC bus) with respect to ground. The advantage is that there is no active signal to cause any interference, but fault location is a challenge with this method as well.
- 3. Passive current monitoring through use of a ground neutral ground reference. The Littelfuse SE-601 Series DC Ground-Fault Monitor (Figure 2) can provide such a reference. This approach creates a neutralground point in between the DC bus voltages and looks for leakage current to or from ground. The advantages of this system are that the fault location (positive or negative DC bus) can be determined, there are no active signals to cause interference, and the reference module usually serves to limit fault currents to a safe value. The disadvantage of this method is that a symmetrical fault (a fault of equal resistance to ground on both buses simultaneously) might not be detected.



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Figure 2. The SE-601 DC Ground-Fault Monitor provides sensitive, fast ground-fault protection with nuisance tripping. Ground-fault current is sensed using an SE-GRM Series Ground-Reference Module-a resistor network that limits ground-fault current to 25 mA. The SE-GRM allows an SE-601 to be connected to systems up to 1200 Vdc and potentially higher.

Any current running through to ground requires attention. Sensitive ground fault-relays will pick up leakage currents at 10 mA or even lower. The latest ground-fault relays can pick up levels of fault current as low as 30 milliamps. Typically, a ground reference module is installed between the negative and positive portions of a DC system, the reference model is connected to the relay, and the relay is connected to the ground.

Figure 3. The SE-704 Earth-Leakage Monitor provides both feeder-level protection or individual-load protection.

Although most BESSs are ungrounded, grounded BESSs do exist but require different methods of ground-fault detection. Designers need to weigh the relative merits of an AC ground-fault relay vs. an AC insulation monitor. An AC ground-fault relay, such as the SE-704 Earth-Leakage Relay (Figure 3), offers very sensitive ground-fault detection and can be used on systems with significant harmonic content. The output contacts can be connected for use in protective tripping circuits or in alarm indication circuits. The analog output can be used with a PLC or a meter. In contrast, an AC insulation monitor such as the PGR-3200 Series Insulation Monitor (Figure 4) which operates on one- or threephase ungrounded systems up to 6 kV, can also be used on grounded systems to monitor the insulation for damage when the system is de-energized.

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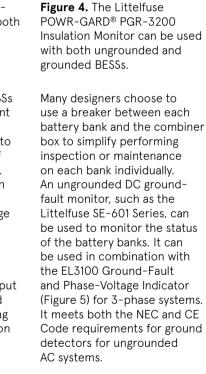


Figure 5. EL3100 Ground-Fault and Phase-Voltage Indicator can be used in conjunction with an SE-601 Series DC Ground-Fault Monitoring for monitoring the status of a BESS's battery banks.





ARC-FLASH PROTECTION

According to OSHA, arc-flash events are responsible for approximately 80 percent of electrically related accidents and fatalities among qualified electrical workers. Even when there are no injuries to workers, an arc flash can destroy equipment, requiring costly replacement and system downtime.

The high levels of DC power that feed into inverters from the combined output of the banks of DC batteries creates the potential for arc-flash incidents. When the outputs of multiple daisy-chained batteries are brought together in a combiner box, they can also produce sufficient DC voltage to initiate an arc. Unlike with sinusoidal AC power, where the zero crossing helps AC arcs extinguish themselves, there's less chance that DC arcs from batteries will be self-extinguishing,

Arc flashes present a number of hazards. The heat can be more intense than the temperature on the surface of the sun, and the accompanying explosion may hurl debris at the speed of a bullet. The threat to both maintenance personnel and nearby equipment is obvious. To mitigate these hazards, arc-flash relays are designed to detect the light from an emerging arc flash and trip an upstream circuit breaker as quickly as possible. For example, the PGR-8800 Series Arc-Flash Relay (Figure 6a) can detect and send a trip signal in less than 1 millisecond, preventing an arc from growing into a potentially catastrophic incident. The trip time for a typical AF0100 Series Arc-Flash Relay (Figure 6b) configuration is less than 5 milliseconds.

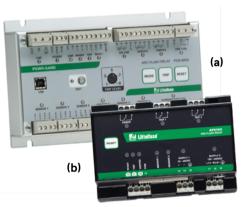


Figure 6. The PGR-8800 Series Arc-Flash Relay (a) detects developing arc-flash incidents by looking for a combination of excess light and current. An optical sensor and adjustable trip level reduce the chance of nuisance tripping by setting a threshold for ambient light. The AF0100 Series Arc-Flash Relay (b) reduces arc-fault damage by detecting the light from an arc flash and rapidly tripping. Two remote light sensors can be connected to one relay and multiple AF0100 and/or AF0500 (not pictured) relays can be connected to monitor additional sensors.

Installing an arc-flash relay system involves placing light sensors around the interior of the enclosure that houses the inverter and the associated bus bars most likely to be the origin of an arc. The power semiconductor device inside the inverter usually fails safe, but it is possible that it or its connectors could fail to ground and cause an arc flash.

ARC-FLASH CONSIDERATIONS FOR DC AND ENERGY STORAGE APPLICATIONS

Allow calculating the arc flash potential for to develop the It's also important to keep in mind for incident energy calculations that battery cabinets tend to direct the energy out of the cabinet calculations for arc-flash incident energy on, particularly the development of IEEE 1584 (Guide for Performing Arc-Flash Hazard door. Large-scale BESS enclosures can expose personnel to even Calculations). A revision is forthcoming based on further testing more energy during an arc flash, both by containing the fault and with AC systems. However, DC arc flash has been less studied and by making it more difficult for workers to self-rescue within a is less understood. The DC fault currents can be released rapidly typical two-second window. on almost all types of BESSs, but those employing Lithium-Ion batteries can release very large amounts of current very rapidly.

The battery banks themselves represent an arc-flash protection challenge in a BESS. An arc flash on one battery bank will be The purpose of arc-flash calculations is to determine the largest fed from other parallel battery banks. This can be resolved possible incident energy. However, a few factors that may not be by monitoring the battery bank and disconnecting from the intuitively obvious can result in higher incident energy levels than bus on a fault. At this point, the arc fault is only fed from the faulted bank, reducing its total energy by a factor proportional would be anticipated if only an overcurrent protective device to the total number of parallel battery banks. The remaining were used: battery banks continue supplying or being supplied with energy. Although disconnecting a faulted bank has a significant impact **Battery age:** As batteries age, their internal impedance on operations and reducing incident energy, a fault local to the increases. This can result in lower arc-flash current, which battery bank is more difficult to address. One option is to provide can in fact lead to higher energy because the overcurrent the means to disconnect/de-couple sections of the battery bank protection device takes longer to operate. physically, further reducing the voltage of each remaining section and reducing the hazard and available incident energy while **State of charge:** A partially depleted battery bank may not

- produce full arcing or short-circuit current. Using an arc-flash relay instead of relying on overcurrent protection devices alone for arc-flash protection can help designers realize a consistently low incident energy throughout the lifetime of the BESS.

To learn more about Analog Devices Supercapacitor Backup Regulator Solutions please



maintenance is being performed.